Table I
Experimental Data

|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mole $\mathrm{HClO}_{4}=$ mole $\mathrm{Pb}\left(\mathrm{ClO}_{4}\right)_{2}$ | $E_{0}, \mathrm{muv}$. | $E^{\prime}$ | $\begin{gathered} \mathrm{HClO}_{4} \\ \text { mole } \\ \text { (per } \end{gathered}$ | $\left(\mathrm{ClO}_{4}\right)_{2}$, mole of $\mathrm{H}_{2} \mathrm{O}$ ) | $E_{c}$ | $E_{0}$ |
| 0.1 | $1.432 \pm 3$ | 1.461 | 0.25 | 0.01 | 1.501 | 1.475 |
| . 025 | $1.417 \pm 3$ | 1.464 | . 25 | . 001 | 1.523 | 1.467 |
| . 1 | $1.407 \pm 3$ | 1.466 | . 25 | . 0001 | 1.549 | 1.464 |
| . 0025 | $1.389 \pm 2$ | 1.467 |  |  |  |  |
| . 001 | $1.378 \pm 2$ | 1.467 |  |  | $E_{0}$ ave | 1.469 |

$E_{0}$ by extrapolation of $E^{\prime} 1.467$

## Summary

1. The possible sources of error in the previous work on the lead dioxide electrode have been discussed.
2. The work of former investigators who found the first stable value of electrolytically prepared lead dioxide to agree within one or two millivolts with the potential of that obtained from chemical sources has been checked.
3. An attempt has been made to explain the high initial value and the final drop in potential of electrolytic lead dioxide. The factors involved in lengthening the stable period of this lead have also been studied.
4. The effect of lead perchlorate on the hydrogen electrode has been investigated and found to be proportional to the $\mathrm{Pb}^{++}$concentration.
5. The standard oxidation potential of $\mathrm{Pb}^{++}-\mathrm{PbO}_{2}$ in molal $\mathrm{H}^{+}$has been measured by two methods and found to be $1.467 \pm 0.003$ volts.

Lincoln, Nebraska
[Contribution from the Research Laboratory of Physical Chemistry, Massachusetts Institute of Technology, No. 205]

## SOME OF THE THERMODYNAMIC PROPERTIES OF AMMONIA.

I. THE COMPRESSIBILITY OF AND AN EQUATION OF STATE FOR GASEOUS AMMONIA. THE VAPOR PRESSURE OF LIQUID AMMONIA

By James A. Beattie and Charles K. Lafrence<br>Received June 20, 1929 Published January 8, 1930

## 1. Introduction

The compressibility of gaseous ammonia is of interest because the curvature of the isometries is greater than for any other gas, except steam, for which there is a considerable body of data. The earlier measurements either do not extend over a very wide range, or the volumes were uncertain. Roth ${ }^{1}$ studied the pressure-volume-temperature behavior of ammonia from 30 to $180^{\circ}$, but his volumes were not definitely determined;
${ }^{2}$ Roth, Wied. Ann., 11, 1 (1880).

Brownlee, Babcock and Keyes ${ }^{2}$ measured the compressibility for two isotherms, and determined the values of the constants of the Keyes equation of state for ammonia from the existing data, and Keyes ${ }^{3}$ presented data for five isometries extending from 39 to 55 cc . per gram and from 60 to $164^{\circ}$. Holst ${ }^{4}$ measured the pressure at several volumes and temperatures from 24 to $100^{\circ}$ and from 3 to 21 atmospheres; and Bridgman ${ }^{5}$ investigated the high pressure field from 1000 to 12,000 atmospheres for the temperature $30^{\circ}$.

Meyers and Jessup ${ }^{6}$ of the Bureau of Standards made a study of the compressibility of ammonia in the low pressure region. The measurements were made by the isometric method and extended from 85.5 to 1300 cc. per gram and from -35 to $+300^{\circ}$. These data will be discussed in a later section.

In the present paper there is presented a series of pressure-volumetemperature measurements on gaseous ammonia, extending from 20 to 95 cc . per gram and from 75 to $325^{\circ}$. These data and those of Meyers and Jessup are correlated by means of an equation of state.

The vapor pressure of liquid ammonia has been measured by Cragoe, Meyers and Taylor ${ }^{7}$ of the Bureau of Standards from -80 to $+70^{\circ}$; and by Keyes and Brownlee ${ }^{8}$ from the boiling point to the critical point. The data of the authors, which extend from 30 to $132^{\circ}$, agree very well with those of the Bureau of Standards and fairly well with the values of Keyes and Brownlee.

## 2. The Experimental Method

All of the measurements were made by the isometric method, the details ${ }^{9}$ of which have been described in a paper on the compressibility of gaseous ethyl ether. Some modifications in the apparatus however deserve to be mentioned.
${ }^{2}$ (a) Brownlee, Babcock and Keyes, Proceedings of the Third International Congress Refrig., Vol. II, p. 189 (1913); also Keyes, Am. Soc. Refrigerating Eng. J., 1, 9 (1914); (b) Keyes and Brownlee, "The Thermodynamic Properties of Ammonia," John Wiley and Sons, Inc., New York, 1916, p. 20.
${ }^{3}$ Keyes, Am. Soc. Refrigerating Eng. J., 7, 371 (1921).
${ }^{4}$ Holst, Bull. Assoc. International Froid., 6, 48 (1915).
${ }^{5}$ Bridgman, Proc. Nat. Acad. Sci., 9, 370 (1923).
${ }^{6}$ Meyers and Jessup, Refrig. Eng., 11, 345 (1925). The compressibility of liquid ammonia between saturation and 50 atmospheres is given in Circular of Bureau of Standards, No. 142, Table 4.
${ }^{7}$ Cragoe, Meyers and Taylor, This Journal, 42, 206 (1920); Scientific Papers of the Bureau of Standards, 16, 1 (1920).
${ }^{8}$ Keyes and Brownlee, This Journal, 40, 25 (1918). See also Keyes, "International Critical Tables," National Research Council, McGraw-Hill Book Co., 1928, Vol. III, p. 234.
${ }^{9}$ Beattie, This Journal, 46, 342 (1924).

The Thermostat.-A larger thermostat was used in the present investigation. It was a liquid bath 36 cm . in diameter and 75 cm . deep, mineral seal oil being used at the lower temperatures and heavy cylinder oil at the higher temperatures. The stirring was accomplished by three sets of propellers each enclosed in a steel tube and geared together. One of these stirrer casings had a larger tube welded around its lower end, thus forming an annular space about 0.5 cm . in width and 20 cm . long which contained about 200 cc . of mercury. The expansion and contraction of this mercury operated a relay which turned on and off the electric current in the three internal heaters, one of which was placed on the top of each stirrer tube. Sufficient current was constantly passed through external heaters to raise the temperature of the bath to within about $2^{\circ}$ of the desired value. The temperature regulation was $\pm 0.001^{\circ}$ over the entire range from 75 to $325^{\circ}$.

The temperatures were measured by a four-lead potential type platinum thermometer calibrated as described in the earlier paper. All temperatures are on the platinum scale.

The Pressure Gage.-The gage had been modified somewhat ${ }^{10}$ and was calibrated against the vapor pressure of carbon dioxide at $0^{\circ}$, this value being taken as 34.401 atmospheres. ${ }^{11}$

The volume measuring device and piezometer were the same as those used in the measurements on ethyl ether but the connecting and riser block was simplified so that only one steel stopcock was used in the entire volume measuring system.

## 3. Filling the Piezometer

A commercial sample of liquid ammonia was allowed to stand in a vessel containing sodium for about three months, the gas phase being removed from time to time by "blowing off." The method of filling the glass piezometer was the same as that used for ethyl ether. The ammonia was distilled eight times, the first and last portion being rejected each time, and the ammonia frozen while the entire system was evacuated after each distillation. It was finally distilled into the glass bomb, which had been evacuated for six days, first at $400^{\circ}$ and later at $350^{\circ}$. The ammonia was then frozen by liquid air and the bomb sealed. The amount of ammonia used was determined by weighing against a counterpoise which had approximately the same outside and inside volume as the bomb. The counterpoise was evacuated when weighing the loaded bomb so that the buoyancy correction was small.

After each loading the vapor pressure of ammonia was measured at $30^{\circ}$. No increase in vapor pressure was observed even when the gas space was reduced to 0.1 or 0.2 cc . In one case after the gas phase bad been completely collapsed, it did not re-form for some minutes even though the external pressure was reduced to less than one atmosphere. After each series of measurements the vapor pressure was determined again but no evidence of a decomposition of the ammonia could be detected.

The method of calculation of the results has been fully described elsewhere. ${ }^{9}$ All volumes are relative to those of mercury, whose density at one atmosphere and various temperatures was calculated from the Callendar and Moss equation. ${ }^{12}$ The temperature coefficient of the compressibility of mercury used was

$$
\frac{1}{V_{0}} \frac{d}{\mathrm{~d} p}\left(\frac{\mathrm{~d} V}{\mathrm{~d} T}\right)=5 \times 10^{-9} \text { atmospheres }{ }^{-1} \text { degrees centigrade }{ }^{-1}
$$

[^0]The measured pressures were corrected for the vapor pressure of mercury. For this purpose the saturated vapor pressures of Smith and Menzies ${ }^{13}$ were used and a correction applied by the Poynting relation for the effect of pressure on vapor pressure.

Two runs were made: one extending from 95 to 35 cc . per gram, and the other from 40 cc . per gram to higher densities. In this latter run a leak developed at the higher pressures, so that the measurements at densities higher than 20 cc . per gram are too uncertain to include in the data, and the pressures of the 20 cc . per gram isometric may be in error by several tenths of an atmosphere.

## 4. Discussion of the Experimental Data

The data are given in Table II, in which the measurements of Meyers and Jessup are also included. Since these two sets of results cover different density ranges, they can only be compared by means of some smoothing function, and for this correlation the Beattie-Bridgeman equation of state ${ }^{14}$ is used.

The method of determining the values of the constants from the experimental data has been given elsewhere. ${ }^{14 b}$ In Table I are given the form of the equation of state and the values of the constants in several sets of units. In the evaluation of the constants most weight was given to the authors' data, as they are at the higher densities. The comparison of the observed and calculated pressure is given in Table II, from which it can be seen that the average deviation of the equation from the measured values is 0.037 atmosphere or $0.077 \%$ for the author's data, and 0.012 atmosphere or $0.155 \%$ for Meyers and Jessup's data.

Table I
Values of the Constants of the Beattie-Bridgeman Equation of State for Ammonia

|  |  | $p=\frac{R}{R}$ | $\left.\frac{(1-\epsilon)}{V^{2}} \right\rvert\, V$ | $B]-\frac{A}{V^{2}}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $R$ | $A=$ | - $-a / V$ | $\underset{B_{0}}{B}=B_{0}$ | $-b / V)$ | $=c / V T_{c}^{3}$ | Mol. wt. |
|  | s: atm | eres; cc | r gram; | ( $T^{\circ} \mathrm{K}$ | $t^{\circ} \mathrm{C} .+273$. |  |
| 4.81824 | 8250 | 10 | 2.005 | 11.222 | $280 \times 10^{6}$ | 17.0311 |
|  |  | ts: at | heres; | per mo |  |  |
| 0.08206 | 2.3930 | 0.17031 | 0.03415 | 0.19112 | $476.87 \times 10^{4}$ | 17.0311 |
|  | s: atmo | res; $V$ | 1 at $0^{\circ} \mathrm{C}$. | 1 atm.; | (Amagat un |  |
| 3.71274 | 4.8986 | 7.706 | 1.5451 | 8.647 | 215.76 | 17.0311 |
| $\times 10^{-3}$ | $\times 10^{-3}$ | $\times 10^{-3}$ | $\times 10^{-3}$ | $\times 10^{-3}$ | $\times 10^{3}$ |  |

[^1]
## Table II

Comparison of the Pressures Calculated from tie Equation of State with the Observed Pressures
For each temperature the first line gives the observed pressure and the second line gives the observed minus the calculated pressure. The equation used for the calculated pressures is given in Table $\mathbf{I}$.

| Volume | c./g. | 95 | 90 | 80 | 70 | 60 | 50 | 45 | 40 | 35 | 30 | 25 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Temp., |  |  |  |  |  |  | Pressures | n atmos |  |  |  |  |  |
| 325 | Obs. | 29.59 | 31.22 | 35.04 | 39.90 | 46.34 | 55.24 | 61.11 | 68.36 | 77.59 | 89.69 | 106.25 | 130.40 |
|  | Obs.-calcd. | -0.07 | -0.05 | -0.03 | -0.03 | -0.01 | 0.00 | 0.02 | 0.02 | 0.05 | 0.08 | 0.10 | 0.12 |
| 300 | Obs. | 28.29 | 29.84 | 33.45 | 38.08 | 44.18 | 52.62 | 58.16 | 65.03 | 73.68 | 85.09 | 100.61 | 123.10 |
|  | Obs.-calcd. | -0.04 | -0.02 | -0.03 | -0.02 | -0.01 | 0.01 | 0.01 | 0.03 | 0.00 | 0.05 | 0.05 | -0.02 |
| 275 | Obs: | 26.98 | 28.44 | 31.87 | 36.25 | 42.00 | 49.96 | 55.18 | 61.62 | 69.77 | 80.45 | 94.88 | 115.67 |
|  | Obs.-calcd. | -0.01 | -0.01 | -0.01 | -0.01 | 0.02 | -0.01 | -0.01 | -0.01 | -0.01 | 0.04 | -0.01 | -0.16 |
| 250 | Obs. | 25.64 | 27.01 | 30.27 | 34.39 | 39.83 | 47.33 | 52.22 | 58.26 | 65.86 | 75.74 | 89.11 | 108.18 |
|  | Obs.-caled. | -0.01 | -0.02 | 0.00 | -0.01 | 0.00 | 0.02 | 0.02 | 0.03 | 0.03 | 0.02 | -0.01 | -0.21 |
| 225 | Obs. | 24.30 | 25.59 | 28.64 | 32.54 | 37.64 | 44.63 | 49.20 | 54.81 | 61.85 | 70.97 | 83.21 | 100.51 |
|  | Obs.-calcd. | 0.00 | -0.01 | -0.01 | 0.01 | 0.01 | 0.02 | 0.02 | 0.03 | 0.03 | 0.02 | -0.03 | -0.27 |
| 200 | Obs. | 22.93 | 24.15 | 27.01 | 30.64 | 35.40 | 41.89 | 46.12 | 51.29 | 57.74 | 66.05 | 77.13 | 92.57 |
|  | Obs.-calcd. | -0.02 | -0.01 | -0.01 | -0.01 | 0.00 | 0.00 | 0.01 | 0.01 | -0.01 | -0.03 | -0.10 | -0.39 |
| 175 | Obs. | 21.56 | 22.70 | 25.36 | 28.74 | 33.14 | 39.13 | 43.01 | 47.73 | 53.61 | 61.11 | 70.98 | 84.54 |
|  | Obs.-calcd. | -0.02 | -0.01 | -0.01 | 0.00 | 0.00 | 0.01 | 0.02 | 0.02 | 0.03 | 0.01 | -0.06 | -0.32 |
| 150 | Obs. | 20.18 | 21.23 | 23.70 | 26.81 | 30.86 | 36.33 | 39.85 | 44.11 | 49.36 | 56.01 | 64.65 | 76.24 |
|  | Obs.-calcd. | -0.01 | -0.01 | 0.00 | 0.00 | 0.02 | 0.03 | 0.04 | 0.05 | 0.04 | 0.04 | 0.00 | -0.20 |
| 125 | Obs. | 18.78 | 19.75 | 22.00 | 24.85 | 28.51 | 33.44 | 36.59 | 40.36 | 44.99 | 50.74 | 58.06 | 67.56 |
|  | Obs.-calcd. | -0.01 | 0.00 | -0.01 | 0.01 | 0.01 | 0.03 | 0.05 | 0.05 | 0.08 | 0.09 | 0.08 | -0.05 |
| 100 | Obs. | 17.36 | 18.24 | 20.28 | 22.84 | 26.12 | 30.47 | 33.21 | 36.47 | 40.41 | 45.19 | 51.09 | 58.28 |
|  | Obs.-calcd. | -0.01 | 0.00 | 0.00 | 0.01 | 0.02 | 0.03 | 0.04 | 0.04 | 0.07 | 0.08 | 0.11 | 0.04 |
| 75 | Obs. | 15.90 | 16.68 | 18.50 | 20.76 | 23.61 | 27.34 | 29.65 | 32.35 | 35.52 |  |  |  |
|  | Obs.-calcd. | -0.01 | 0.00 | -0.01 | -0.01 | -0.02 | -0.02 | -0.02 | -0.02 | -0.02 |  |  |  |
| 50 | Obs. | 14.37 | 15.05 | 16.62 | 18.54 |  |  |  |  |  |  |  |  |
|  | Obs.-calcd. | -0.05 | -0.06 | -0.07 | -0.09 |  |  |  |  |  |  |  |  |
| Av. de | ( atm .) | 0.022 | 0.017 | 0.016 | 0.018 | 0.011 | 0.016 | 0.024 | 0.028 | 0.034 | 0.046 | 0.055 | 0.178 |
| Av. \% | dev. | 0.101 | 0.076 | 0.070 | 0.073 | 0.035 | 0.045 | 0.059 | 0.060 | 0.067 | 0.076 | 0.077 | 0.191 |
|  |  |  | Total a Total a | verage de | viation ( deviation | (atm.) |  |  |  | $0.037$ |  |  |  |

## Table II (Concluded)

B. Data of Meyers and Jessup

| Volume, cc./g. <br> Temp., ${ }^{\circ} \mathrm{C}$. |  | 1300 | 500 | 300 | 200 | 150 | 115 | 85.5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Pressures in |  |  |  |  |  |  |
| 300 | Obs |  |  | 9.126 | 13.631 | 18.101 | 23.497 |  |
|  | Obs.-calcd. |  |  | -0.004 | -0.008 | -0.010 | -0.009 |  |
| 250 | Obs. |  | 5.007 | 8.308 | 12.395 | 16.439 | 21.305 | 28.378 |
|  | Obs.-calcd. |  | -0.002 | -0.004 | -0.007 | -0.009 | -0.010 | -0.018 |
| 200 | Obs. | 1.747 | 4.519 | 7.489 | 11.153 | 14.766 | 19.098 | 25.361 |
|  | Obs.-calcd. | -0.001 | -0.002 | -0.002 | -0.005 | -0.006 | -0.004 | -0.007 |
| 150 | Obs. | 1.561 | 4.030 | 6.664 | 9.902 | 13.075 | 16.858 | 22.285 |
|  | Obs - calcd. | 0.000 | -0.001 | $-0.003$ | -0.002 | -0.004 | -0.001 | 0.003 |
| 100 | Obs. | 1.374 | 3.537 | 5.832 | 8.632 | 11.352 | 14.567 | 19.109 |
|  | Obs.-calcd. | -0.001 | -0.002 | -0.002 | -0.002 | -0.004 | 0.001 | 0.003 |
| 50 | Obs. | 1.187 | 3.039 | 4.985 | 7.327 | 9.567 | 12.162 | 15.722 |
|  | Obs - calcd. | 0.000 | -0.003 | $-0.005$ | -0.009 | -0.017 | -0.027 | -0.058 |

$\begin{array}{lrrrrrrr}\text { Av. dev. (atm.) } & .001 & 0.005 & 0.009 & 0.012 & 0.018 & 0.023 & 0.018 \\ \text { Av. } \% \text { dev. } & .073 & .173 & .180 & .168 & .186 & .194 & .098\end{array}$
Total average deviation (atm.)
Total average $\%$ deviation

35 Obs.
Obs. - calcd.
Obs. - calcd.
25 Obs. $\quad 1.092 \quad 2.786 \quad 4.549 \quad 6.645 \quad 8.618$
Obs.-calcd. $-0.001-0.005-0.012-0.026-0.052$
15 Obs.
Obs. - calcd
Obs.-calcd
5 Obs.
Obs.-caled.

$$
6.361
$$

0 Obs. $\quad 0.997 \quad 2.528$
-10 Obs.
$\begin{array}{rr}-0.001 & -0.009 \\ 2.421\end{array}$
Obs. - calcd
$-0.014$
11.391
$-0.061$

$$
-0.040
$$

10 Obs.

Obs.-calcd. $-0.001-0.009$
-20 Obs. 0.921

Obs. - calcd. -0.002
8.81211 .129
$-0.043-0.074$
4.279

$$
-0.021
$$

$$
4.188
$$

$$
-0.024
$$

Obs.-caled. -0.001
-30 Obs. 0.882
-35 Obs. .865
Obs.-calcd. . 000
$\square$
.
$\square$
Obs.-calca
$\square$
$\square$
sets of measurements which is evident when the A and B functions are plotted against the density. Hence an equation was passed through the Bureau of Standards data alone. The values of the constants and a comparison of the observed and calculated pressures are given in Table III. The average deviation is 0.004 atmosphere or $0.043 \%$. The great

Table III
Comparison of the Pressures Calculated from the Special Equation of State for the Data of Meyers and Jessup with the Observed Pressures
The calculated pressures were computed with the values of the constants given below, which were obtained from a consideration of the data of Meyers and Jessup alone. The values of the constants (see Table I for the form of the equation) in units of cc. per gram, atmospheres, ${ }^{\circ} \mathrm{C} .\left(T^{\circ} \mathrm{K} .=t^{\circ} \mathrm{C} .+273.13\right)$ are

| $R$ | $A_{0}$ | ${ }^{a}$ | $B_{0}$ | $b$ | ${ }^{c}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 4.81824 | 3000 | 51.5 | 0.45 | 131 | $360 \times 10^{6}$ |

The observed pressures are given in Table IIB

| Volume, cc./g. | 1300 | 500 | 300 | 200 | 150 | 115 | 85.5 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Av. dev. (atm.) | 0.000 | 0.001 | 0.002 | 0.004 | 0.005 | 0.009 | 0.007 |
| Av. $\%$ dev. | .032 | .046 | .047 | .045 | .040 | .059 | .032 |
| Total average deviation (atm.) |  |  |  | 0.004 |  |  |  |
| Total average $\%$ \% deviation |  |  |  | .043 |  |  |  |

difference in the values of the constants for these data may be due either to the fact that the Bureau of Standards measurements are at low pressures where a very slight difference in trend causes a large change in the values of the constants or to the failure of the equation of state to represent the data near saturation within the experimental error, when the constants are determined from measurements at higher temperatures and pressures. It is probable that both of these factors enter into the present case, but it should be emphasized that the authors' data and those of Meyers and Jessup are in excellent agreement, and that the equation of state has reproduced these data very well.

## 5. Weight of a Normal Liter of Ammonia

The weight of a liter of a gas at $0^{\circ}$ and one atmosphere, usually called the weight of a normal liter, can be calculated from an equation of state and the molecular weight. The weights of a normal liter of several gases ${ }^{15}$ have been evaluated by means of the Beattie-Bridgeman equation of state and agree well with the experimental values. By use of the same method the weight of a normal liter of ammonia was computed using the molecular weight 17.0311 and the comparison with the observed values is given in Table IV. The experimental values are those selected by Blanchard and Pickering, ${ }^{16}$ who make no attempt to explain the difference between the weight obtained at the Bureau of Standards, which is the result of two different investigators, and those of other careful observers, which

[^2] (1926).
are all very close to 0.7708 . The equation based on the authors' determinations of the compressibility of ammonia leads to the value 0.7706 , in good agreement with the earlier data; that based on the data of Meyers and Jessup gives a value of the normal density of 0.7715 , agreeing with the Bureau of Standards measured value.

The weight of a normal liter obtained by Keyes ${ }^{2 b}$ from his equation of state is 0.7699 g .

Table IV
Weight of a Normal Liter of Ammonia Source

Grams per liter
Calculated from values of constants of Table I 0.7706

Average of experimental values exclusive of those of Bureau of Standards . 7708
Calculated from value of constants of Table III .7715
Bureau of Standards experimental value .7713

## 6. The Vapor Pressure of Liquid Ammonia

The glass bomb was loaded with about 9 g . of liquid ammonia in the same manner as for a compressibility run. The vapor pressure was measured from 30 to $132^{\circ}$. At each temperature the volume of the vapor space was varied from about 80 cc . to less than 1 cc . Thus at $30^{\circ}$ the following values were obtained.

| Volume of vapor space (cc.) | 76 | 5 | 2.4 | 1.8 | 0.8 | 0.2 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Vapor pressure (atm.) | 11.517 | 11.514 | 11.515 | 11.515 | 11.516 | 11.515 |

These values show that no inert gas was present as there is no increase of the vapor pressure with decrease in volume of the vapor space.

The results are given in Table V, in which are included the measurements made at the Bureau of Standards, ${ }^{7}$ and those by Keyes and Brownlee. ${ }^{8}$ The agreement with the pressures determined at the Bureau of Standards is better than $0.1 \%$, the authors' pressures being higher, but this difference cannot be explained on the basis of permanent gas in the authors' ammonia since the pressure did not increase with decrease of the vapor volume.

Table V
Vapor Pressure of Liquid Ammonia

| Temp., <br> ${ }^{\circ} \mathrm{C}$. | Vapor pressure in atmospheres <br> Beattie and <br> Lawrence | Bureau of <br> Standards | Keyes and <br> Brownlee | Temp. <br> ${ }^{\circ} \mathrm{C}$. | Vapor pressures in atmospheres <br> Beattie and <br> Lawrence | Keyes and <br> Brownlee |
| :---: | :---: | :---: | :---: | :---: | :---: | :--- |
| 30 | 11.515 | 11.512 | $\ldots$. | 100 | 61.779 | 61.816 |
| 40 | 15.343 | 15.339 | $\ldots$. | 110 | 74.83 | 74.84 |
| 50 | 20.074 | 20.059 | $\ldots$. | 120 | 89.98 | 89.80 |
| 60 | 25.815 | 25.797 | $\ldots$. | 125 | 98.45 | 98.08 |
| 70 | 32.717 | 32.687 | $\ldots$. | 130 | 107.6 | 106.9 |
| 80 | 40.894 | $\ldots \ldots$ | 40.902 | 131 | 109.6 | 108.8 |
| 90 | 50.526 | $\ldots$. | 50.558 | 132 | 111.5 | 110.6 |

## 7. Summary

The compressibility of gaseous ammonia has been determined from 20 to 95 cc. per gram and from 75 to $325^{\circ}$. These data agree with the
measurements of Meyers and Jessup, which extend from 85.5 to 1300 cc . per gram to better than $0.1 \%$. The constants of the Beattie-Bridgeman equation of state have been determined from these data and their values are given in Table I. The equation of state reproduces the data of the authors with an average deviation of 0.037 atmosphere, or $0.077 \%$ and the data of Meyers and Jessup to 0.012 atmosphere or $0.155 \%$.

An equation was passed through the Meyers and Jessup data alone, which represents them to 0.004 atmosphere, or $0.043 \%$.

The weight of a normal liter of ammonia calculated from the equation based on the authors' work is 0.7706 g . and that calculated from the data of Meyers and Jessup is 0.7715 g . The experimental value determined at the Bureau of Standards is 0.7713 g . and the average of all other careful workers is 0.7708 g .

The vapor pressures of ammonia have been determined from 30 to $132^{\circ}$. They agree very well with the Bureau of Standards values, which extend to $70^{\circ}$, and quite well with those of Keyes and Brownlee above $70^{\circ}$.

Cambridge, Massachusetts
[Contribution from the Department of Chemistry of the University of British Columbia]

# THE EFFECT OF TEMPERATURE ON THE MOLECULAR SURFACE ENERGY OF BINARY MIXTURES. I 

By W. F. Seyer and W. S. Peck

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The surface tension of pure liquids has been a subject of much investigation of late. The molecular surface energy has also received a good deal of attention, though this property has been largely studied from the concentration point of view and little attention has been paid to the effect of temperature on surface energy. It is true that Ramsay and Aston ${ }^{1}$ determined the surface tensions of a few binary mixtures over considerable ranges and from the results concluded that in those cases examined the molecular weight of the mixture could be taken as the mean of the values for the two substances, but their work was limited to mixtures somewhat similar in properties. An extensive series of measurements has been carried out by Kremann and Meingast. ${ }^{2}$ Unfortunately, the temperature interval over which they measured the surface tension was small and consequently little could be learned from their figures in regard to the effect of temperature on the molecular surface energy of binary mixtures.

An interesting series of solubility relationships is that shown by the

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[^0]:    ${ }^{10}$ See Keyes and Dewey, J. Opt. Soc. Am., 14, 491 (1927).
    ${ }^{11}$ O. C. Bridgeman, This Journal, 49, 1174 (1927).
    ${ }^{12}$ Callendar and Moss, Phil. Trans. Roy. Soc., 211, 1 (1912).

[^1]:    ${ }^{13}$ Smith and Menzies, This Journal, 32, 1434 (1910).
    ${ }^{14}$ Beattie and Bridgeman, (a) ibid., 49, 1665 (1927); ibid., 50, 3133 (1928); (b) Proc. Am. Acad. Arts and Sci., 63, 229 (1928).

[^2]:    ${ }^{15}$ Beattie and Bridgeman, This Journal, 50, 3151 (1928).
    ${ }^{16}$ Blanchard and Pickering, Scientific Papers of the Bureau of Standards, 21, 141

[^3]:    ${ }^{1}$ Ramsay and Aston, Proc. Roy. Soc. London, 55, 184 (1894).
    ${ }^{2}$ Kremann and Meingast, Monatsh., 35, 1323 (1914),

